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## Picosecond Avalanche Detector — working principle and gain measurement with a proof-of-concept prototype

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## Picosecond Avalanche Detector — working principle and gain measurement with a proof-of-concept prototype

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**ABSTRACT:** The Picosecond Avalanche Detector is a multi-junction silicon pixel detector based on a (NP)<sub>drift</sub>(NP)<sub>gain</sub> structure, devised to enable charged-particle tracking with high spatial resolution and picosecond time-stamp capability. It uses a continuous junction deep inside the sensor volume to amplify the primary charge produced by ionizing radiation in a thin absorption layer. The signal is then induced by the secondary charges moving inside a thicker drift region. A proof-of-concept monolithic prototype, consisting of a matrix of hexagonal pixels with 100 μm pitch, has been produced using the 130 nm SiGe BiCMOS process by IHP microelectronics. Measurements on probe station and with a <sup>55</sup>Fe X-ray source show that the prototype is functional and displays avalanche gain up to a maximum electron gain of 23. A study of the avalanche characteristics, corroborated by TCAD simulations, indicates that space-charge effects due to the large primary charge produced by the conversion of X-rays from the <sup>55</sup>Fe source limits the effective gain.

**KEYWORDS:** Solid state detectors; Timing detectors; Particle tracking detectors (Solid-state detectors); Pixelated detectors and associated VLSI electronics

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## Contents

<b>1</b>	<b>Introduction</b>	<b>1</b>
1.1	Design challenges of avalanche diodes for picosecond timing measurement with ionizing radiation	1
<b>2</b>	<b>Working principle of the Picosecond Avalanche Detector</b>	<b>2</b>
<b>3</b>	<b>The proof-of-concept PicoAD prototypes</b>	<b>3</b>
<b>4</b>	<b>TCAD simulations</b>	<b>5</b>
<b>5</b>	<b>Probe station measurements</b>	<b>6</b>
<b>6</b>	<b>Measurements with a <math>^{55}\text{Fe}</math> radioactive source</b>	<b>10</b>
<b>7</b>	<b>Conclusions</b>	<b>13</b>

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## 1 Introduction

The monolithic detector presented in this paper, the Picosecond Avalanche Detector (PicoAD) [1], is a multi-junction silicon pixel sensor for the detection of light and ionizing radiation, developed in the framework of the H2020 ERC Advanced MONOLITH project [2]. It is devised to combine the space resolution and high detection efficiency of PIN sensors with picosecond time resolution by enhancing the timing performance by avalanche multiplication in a continuous gain layer implanted deep in the depleted region.

### 1.1 Design challenges of avalanche diodes for picosecond timing measurement with ionizing radiation

Avalanche diodes have been recently used to detect ionizing radiation, exploiting the signal amplification provided by the impact ionization to increase the signal-to-noise ratio and improve the detector time resolution [3–5]. This approach was successful in achieving tens of picoseconds time resolution with Minimum Ionizing Particles (MIPs), but some aspects of the sensor design present challenges: the reach-through structure typically used in N-on-P diodes to localize the gain layer underneath the pixel is susceptible to the strong variations of the electric field at the pixel edge, requiring to introduce discontinuities of the gain layer in the inter-pixel regions, which could impact the sensor detection efficiency and time resolution. This problem is often mitigated by increasing the pixel size to reduce the fraction of the sensor inactive area [5, 6].<sup>1</sup> Another challenge to the

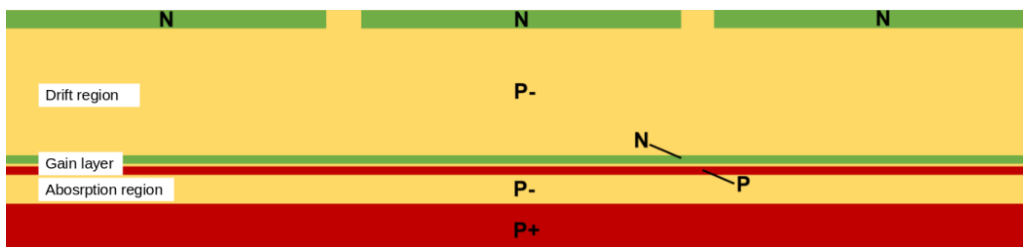
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<sup>1</sup>Other solutions to increase the fill factor of small pixel sensors with gain exist, like the use of deep trenches to achieve pixel isolation with limited dead area [7] or AC coupling of the readout on uniform gain layers [8], but these solutions are not available in most CMOS processes.

development of this technology is the presence of charge-collection noise [9], which produces an intrinsic time jitter during the collection of the signal charge, generated by the fluctuations of the charge profile along the path of the primary ionization. This effect can be reduced by thinning the avalanche diode, [4, 9, 10] at the cost of increasing the detector capacitance and consequently the time jitter of the front-end electronics. Charge-collection noise thus makes it difficult to achieve time resolutions below 20 ps for MIPs with present avalanche diodes. The reason is mostly due to the fact that the region where the primary charge is produced coincides with the region where the secondary charges drift and contributes to most of the induced signal.

## 2 Working principle of the Picosecond Avalanche Detector

The PicoAD introduces design flexibility to the avalanche-based sensors by moving the gain layer away from the pixel matrix and separating the region where the primary charge is produced and amplified from the region dedicated to the signal induction on the readout electrodes. Figure 1 shows the cross section of the PicoAD. The detector is characterized by a fully depleted multi-junction  $(NP)_{\text{pixel}}(NP)_{\text{gain}}$  structure, which provides a new degree of freedom for the engineering of the electric field. Indeed, when the bias voltage is applied, the sensor depletion region expands from the two junctions that operate in inverse polarization: the one close to the top surface (pixel junction) serves to isolate the pixels, and the one close to the bottom edge of the depletion region (gain junction) provides an electric field large enough to generate impact ionization and, therefore, avalanche gain. The central, direct junction is isolated by the other two junctions until full depletion is achieved.



**Figure 1.** Simplified cross section of the PicoAD detector. The sensor presents N-type pixels on a high-resistivity epitaxial layer with boron background. A second junction, deep inside the sensor volume, is used to produce a continuous avalanche gain layer. The epitaxial layer and the deep junction are operated in full depletion.

When crossed by ionizing radiation, the primary holes generated inside the region that extends between the pixel and gain junctions will drift towards the gain junction, featuring little or no amplification in silicon, while the primary electrons generated below the gain junction will drift upwards to be amplified, producing secondary charges. This behavior allows identifying three main regions:

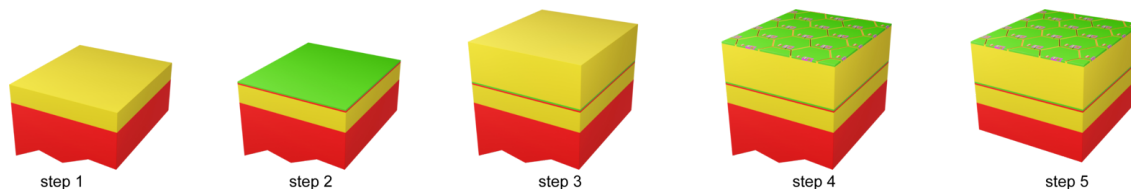
- The primary *absorption region*, constituted by the bottom P- doped region, near the backside contact. This region does not produce impact ionization itself, but the  $e^-$  signal generated here will be amplified by the PicoAD.
- The uniform and continuous deep NP junction is the *gain layer*, operated in proportional mode and therefore free from dark noise counts when detecting ionizing radiation.

- The *drift region*, which corresponds to the thicker top P- doped region, between the pixels and the gain layer. Primary charges and secondary electrons moving in this region induce most of the signal current in the pixel above, according to the Shockley-Ramo theorem [11, 12].

This sensor structure offers multiple advantages:

- First and foremost, the gain layer is a uniform implant far from the pixels, therefore it is less subject to strong variations of the electric field, and can grant uniform signal amplification on all the detector surface. This characteristic enables the possibility to reduce the pixel size with less impact on the avalanche gain performance, as long as the inter-pixel distance is smaller than or comparable to the drift-region thickness.
- Another advantage is that the absorption region can be made arbitrarily thin to reduce the charge-collection noise without significantly increasing the pixel capacitance. This is a fundamental feature because it allows exploiting the advances in fast, low-noise electronics to boost the signal-to-noise ratio and achieve picosecond time resolution.
- Finally, the design of the pixel matrix does not depend on the presence of the gain layer. This makes the R&D simpler because it allows integrating the PicoAD gain layer in an existing sensor design.

The distinctive characteristics of the PicoAD is its multi-junction structure. It requires the implantation of uniform, deep NP doping profiles to generate the gain layer close to the backside surface of the sensor depleted region. Given the thin depletion region required to achieve picosecond time resolution, a possible approach for manufacturing the PicoAD is producing special epitaxial wafers that integrate the gain structure before the surface processing of the wafer. The procedure adopted for the manufacturing of the proof-of-concept prototype is depicted in figure 2



**Figure 2.** Manufacturing process of the PicoAD. Step 1: a high-resistivity epitaxial (absorption) layer is grown on a low resistivity, boron-doped substrate. Step 2: a uniform NP gain layer is implanted. Step 3: a second epitaxial layer is produced, which corresponds to the sensor drift region. Step 4: the top surface is processed to produce the pixel matrix; in the case of a monolithic implementation of the PicoAD, this is a full-CMOS processing. Step 5: the substrate can be thinned from the backside and metallized.

### 3 The proof-of-concept PicoAD prototypes

Proof-of-concept PicoAD prototypes were produced in a monolithic implementation by the Leibniz Institute for High Performance Microelectronics (IHP). The manufacturing of the prototypes was divided in wafer preparation and CMOS processing using their SG13G2 130nm SiGe BiCMOS process.

**Wafer preparation.** The PicoAD was produced on boron-doped substrates with a resistivity of  $0.1 \Omega\text{cm}$ . To guarantee the uniformity of the electric field in the gain layer, the drift region of the PicoAD should be thicker than the inter-pixel distance of the matrix. This condition was not compatible with a full depletion of the sensor using the epitaxial process with the minimum boron concentration of  $3 \cdot 10^{14} \text{cm}^{-3}$  available at IHP at the time of manufacturing. For this reason, the prototype wafer produced was made by a  $5 \mu\text{m}$  thick epitaxial layer under the gain layer (absorption region) and a  $10 \mu\text{m}$  thick epitaxial layer above the gain layer (drift region). The thickness of the drift region of this proof-of-concept PicoAD prototype is thus sub-optimal, and may lead to a reduction of the avalanche gain and a distortion of the weighting field responsible for signal induction in the inter-pixel region.<sup>2</sup>

Four implantation doses were used to form the gain layer (dose 1 being the lowest, dose 4 the highest), targeting a sensor working point at a bias voltage between 100 V and 200 V. In all cases the dose of the P-type implant was set at 60% of the dose of the N-type implant, to guarantee a reduction of the electric field in the absorption region when full depletion is reached.

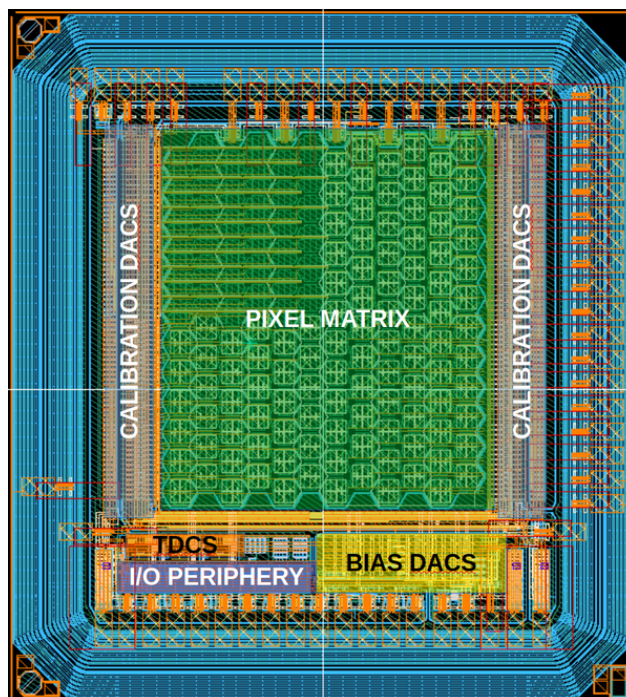
One of the risks associated with the manufacturing of the multi-junction structure is the presence of a direct junction in the transition between the drift and the gain regions. During sensor operation, when the epitaxial layer is fully depleted, this region is emptied of all free charges. But this is not the case during the ramp-up of the sensor bias: at this stage, if the gain layer implantation reaches the edge of the sensor, a conductive path with the substrate may be formed where the silicon is cut, producing an excess current in the device. To avoid this effect it was decided to use an implantation mask to guarantee that the gain layer ended at  $80 \mu\text{m}$  from the chip edge.

The wafers were produced using the process that was available at IHP, which is a dichlorsilane-based process at  $850^\circ\text{C}$ , optimized for sub-micron epitaxial processing. This process could be used to make proof-of-concept prototypes, but it is not suitable for producing large volumes of wafers as it is time consuming and has non-negligible risk of introducing defects on the surface of the thicker epitaxial drift layer.

**CMOS processing.** Due to its thin absorption layer, the PicoAD generates ultra-fast signals that are smaller than those produced by typical avalanche diodes used to detect ionizing particles. For this reason, this sensor should be integrated with ultra-fast, low noise front-end electronics. The best analog performance in terms of speed and noise of the pre-amplification stage can be achieved using Silicon-Germanium Heterojunction Bipolar Transistors (SiGe HBT) [13]. For this reason, the monolithic silicon pixel layout already designed and produced in 130 nm SiGe BiCMOS of IHP for the H2020 ATTRACT MonPicoAD project<sup>3</sup> [14, 15] was used to produce the PicoAD proof-of-concept prototype. The ASIC comprises a matrix of hexagonal pixels of  $65 \mu\text{m}$  side (corresponding to approximately  $100 \mu\text{m}$  pitch), with an inter-pixel distance of  $10 \mu\text{m}$ . Four of the pixels are connected to charge amplifiers with analog drivers, which are used to measure precisely the charge produced in the sensor. Figure 3 shows the layout of the monolithic silicon pixel ASIC.

<sup>2</sup>The thickness of the drift region should be larger than the inter-pixel distance, which is  $10 \mu\text{m}$  in the present prototype.

<sup>3</sup>For the ATTRACT MonPicoAD project, this layout was produced on standard wafers without internal gain and characterised in a testbeam with 180 GeV pions, showing full efficiency and time resolution of 36 ps [14].



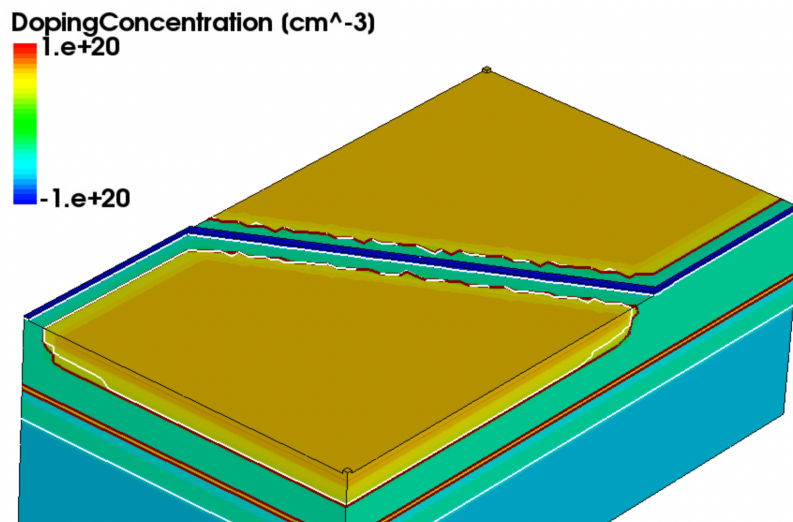
**Figure 3.** Layout of the monolithic silicon pixel ASIC used to test the PicoAD proof-of-concept prototypes. A detailed description of the ASIC layout and operation is reported in [14].

#### 4 TCAD simulations

A study of the expected behavior of the PicoAD proof-of-concept prototypes was carried out using Technology Computer Aided Design (TCAD) simulations. The results refer to a 3D geometry model comprising a quarter of the hexagonal pixel with mirroring boundary conditions, which was used to assess the performance of the sensor at full depletion. Figure 4 shows the model geometry. Quasi-stationary ramp-up of the sensor bias was used to simulate the electric field in the sensor after full depletion of the epitaxial layer (comprising the gain layer). Such simulations show the stationary currents in the sensor, but they do not show the dynamic behavior associated to the removal of free carriers inside the sensor during ramp-up, which will be discussed in section 5 using measurement data.

Figure 5 shows the expected electric field intensity for a fully depleted PicoAD sensor at the highest implantation dose of the gain layer (dose 4). At full depletion, the maximum value of the electric field is observed in the gain layer, with a small drop in the inter-pixel region due to the limited thickness of the drift region and to the presence of the P+ implant (PSTOP) used to stop the formation of a conductive channel under the shallow trench isolation. The field in the drift region, despite showing a gradient due to the relatively low resistivity of the epitaxial layer, is high enough to guarantee saturation of the electron drift velocity over a large fraction of the pixel cell while, as it is the case for this prototype, it is close to saturation even in the region under the PSTOP.

Transient simulations were performed to estimate the avalanche gain inside the sensor at a bias voltage 2.5 V below the gain layer breakdown. For this study, a primary charge of 63 electrons, corresponding to the most probable charge deposited by a MIP in one micron of silicon, was deposited on one-micron-long segments at different depths of the depletion region and the gain was evaluated



**Figure 4.** TCAD 3D model geometry used for simulation of the PicoAD gain with fully depleted sensor. The volume simulated corresponds to one quarter of two adjacent hexagonal pixels.

as the ratio between the collected charge and the primary charge. Figure 6 shows the results of the simulation at the center and at the edge of the pixel (positions C3 and C1 of figure 5, respectively).

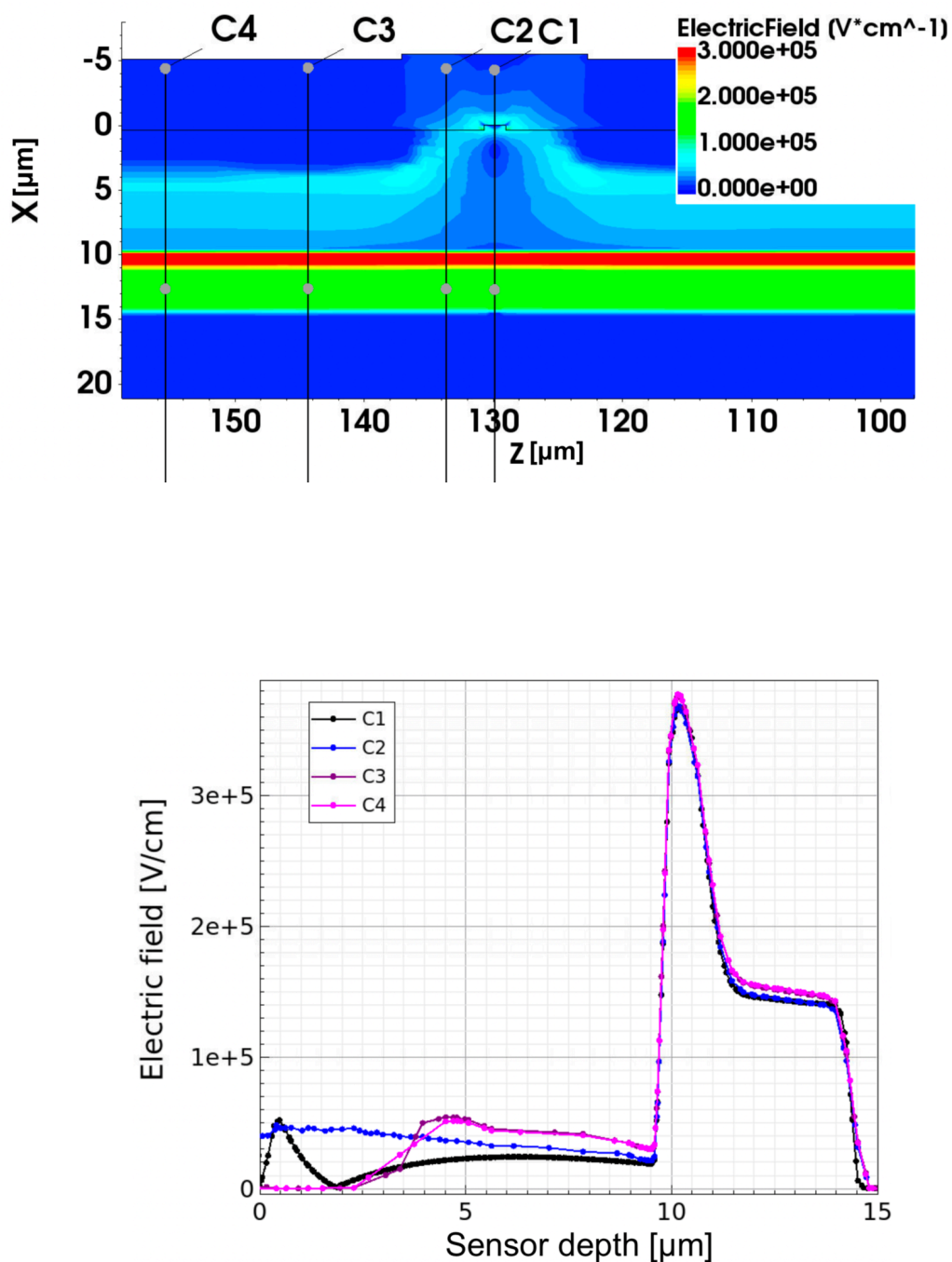
According to design, the PicoAD gain layer amplifies the signal of electrons produced in the absorption region (electron gain), while it produces little to no gain when the primary charge is generated in the drift region (hole gain). It must be noted that the small differences in electric field between the edge and the center of the pixel observed in this prototype (see figure 5) produce a large difference in gain. The impact of these electric-field variations is more severe when the sensor is operated close to breakdown. Despite this, the simulation confirms that the presence of intense electric field in the gain layer both under the pixel and in the inter-pixel region shows that the sensor provides 100% gain fill-factor. Reduction of the ratio between the inter-pixel distance and the epitaxial layer thickness above the gain layer in future PicoAD prototypes will allow better uniformity of the sensor gain.

## 5 Probe station measurements

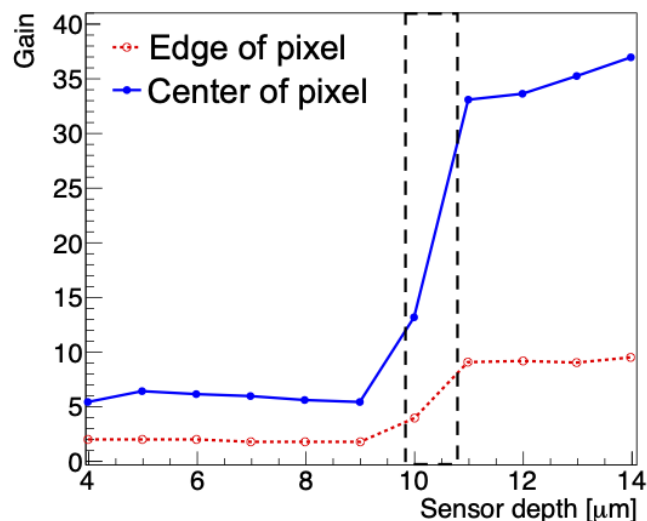
The IV characteristics of the four gain-layer doping doses of the PicoAD proof-of-concept prototypes were measured with the Cascade Microtech CM300 probe station of the cleanrooms of the University of Geneva. For the measurements, the substrate was connected to negative high-voltage, while the deep N-wells forming the pixel matrix and hosting the electronics were connected to ground. The probe station was able to measure the total current (*substrate current*), but also independently the current entering into a sub-matrix of pixels (*pixel current*), the electronic N-wells (*power current*) and the innermost guard-ring (*Guard Ring current*). Figure 7 shows the location on the ASIC surface of the different N-wells as well as the color-code associated to the current readout that will be used in the subsequent figures.

Figure 8 left shows the substrate current as a function of the sensor bias for a prototype chip with dose 1 implant of the gain layer when a negative high voltage from 0 to 90 V was applied and

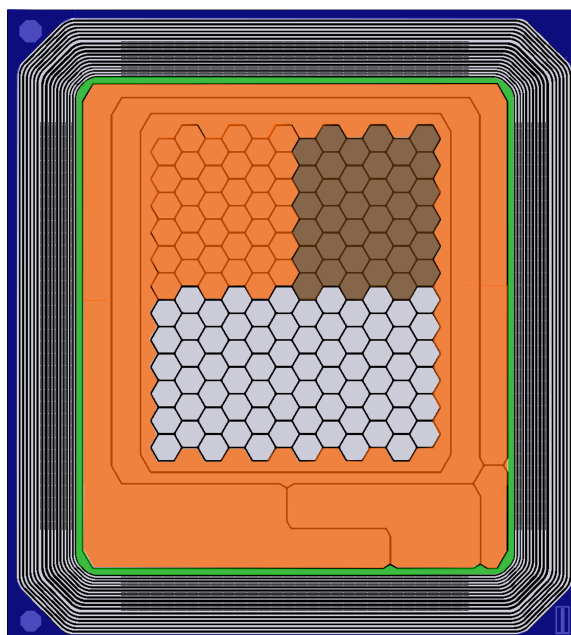




**Figure 5.** (Top) 2D cut of the modulus of the electric field in the sensor volume after full depletion at a bias voltage 2.5 V before breakdown. The vertical lines C1, C2, C3 and C4 represent the regions defining for the 1D cuts used for the study of the electric field: C1 is at the center of the inter-pixel region; C2 at the edge of the collection electrode; C3 is close to the side of the collection electrode; C4 is at the center of the collection electrode. (Bottom) 1D cut of the modulus of the electric field in the four regions of the sensor volume.

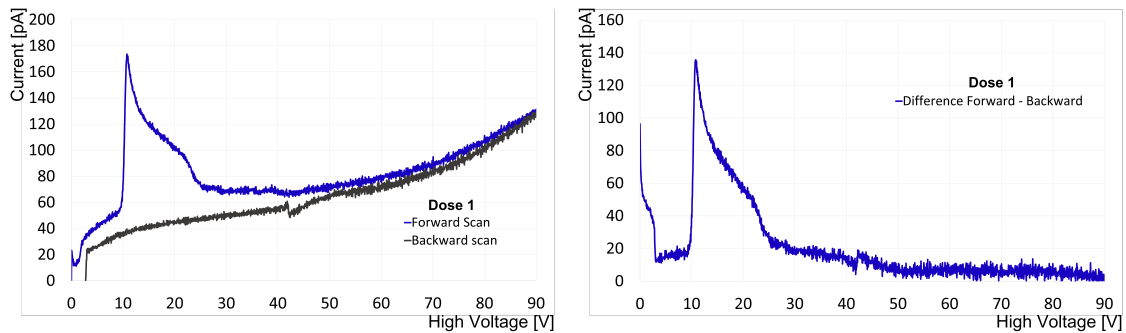


**Figure 6.** Simulation of the gain produced by 63 electrons in a dose 4 PicoAD proof-of-concept prototype as a function of the initial position of the primary charge. The simulation is performed for 1  $\mu\text{m}$  segments of a MIP in two of the cross sections reported in figure 5: C1, edge of the pixel (red dotted line); C3, center of the pixel (blue line). In this prototype, the gain layer is placed at 10  $\mu\text{m}$  depth. The black dashed lines indicate the high field region produced by the gain layer. For a primary electron-hole position between 0 and 10  $\mu\text{m}$  the avalanche is initiated by holes, between 10 and 14  $\mu\text{m}$  the avalanche is initiated by electrons.



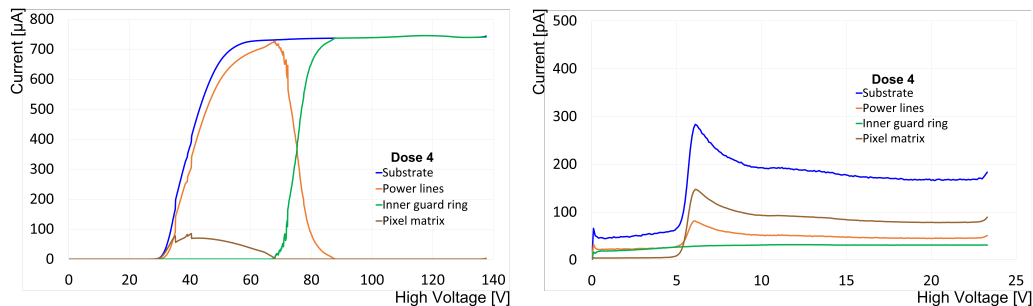
**Figure 7.** The regions of the chip probed in the IV scans. Each color corresponds to a different region for which the current was measured independently. The brown region is one of the matrices of passive pixels. The orange region is the deep N-well that hosts the electronics of the active pixels and the periphery of the chip. The green region probes the current collected by the innermost guard ring. The blue region is the substrate, which was accessible from outside the guard ring on the top surface and from the backside connection. The pixels in grey and the guard rings were left floating.

subsequently ramped down. The sensor breakdown voltage was measured to be 185 V, and thus is not visible in figure 8. The substrate current deviates from a typical monotonic rise, showing a steep increase at 10 V during ramp-up, followed by a reduction and a return to the original trend line at 30 V. This behavior is not present when the voltage is ramped back down. The difference between ramp-up and ramp-down currents is displayed in figure 8 right. The excess current between 10 and 30 V, which cannot be reproduced by TCAD quasi-stationary simulations, can be explained by the presence of free carriers inside the junction formed by the gain layer. Indeed, as soon as the high voltage is applied, the depletion layer starts extending downwards from the pixel junction into the epitaxial layer. During this phase the epitaxial layer above and below the N-type gain-layer implant is referred to negative high voltage, leaving the gain implant isolated with the free charges trapped inside the undepleted N-type gain layer. The removal of these trapped charges produces the measured non-stationary current, that disappears when the PicoAD is fully depleted. The magnitude of the extra current depends on the speed of the high voltage ramp, since it is produced by the removal of a fixed amount of charge.



**Figure 8.** (Left) Substrate current as a function of the sensor bias voltage applied to the substrate of a PicoAD sensor with gain-layer implant dose 1. In blue the current measured during the ramp-up of the high voltage, in black the current during the ramp-down. The reason for the current peak visible between 10 V and 30 V during ramp-up, and not observed during ramp-down of the high voltage, is given in the text. Each point is obtained averaging the current for 0.2 seconds. (Right) Current difference between ramp up and ramp down of the sensor bias voltage.

Figure 9 shows the IV measurement performed on a sample with the highest gain-layer implant dose (dose 4) from the same wafer. In this case, a large extra current was visible after reaching the start of the depletion of the gain layer. The origin of this extra current is attributed to the region outside the guard ring (possibly the chip edge). TCAD simulations suggest that this current could be injected to the pixels and power lines via the undepleted gain layer, which is the case of PicoAD sensors with the gain layer extending under the guard ring. This extra current was mostly observed for samples with larger gain-layer implant dose and with an early onset of the floating N-layer depletion. The presence of local defects in silicon discussed in section 3 could contribute to the activation of this extra current. Figure 9 also shows that, after full depletion of the gain layer, all the excess current is collected by the guard ring and therefore this current has no influence on the sensor performance. This effect can be avoided by removing the part of the gain-layer implant that is underneath the guard ring.



**Figure 9.** IV measurement of a PicoAD sensor with gain-layer implant dose 4. (Left) In blue: the total current collected by the substrate. In brown: the current collected by the pixel terminals. In orange: the current collected by the power lines. In green: the current collected by the innermost guard ring. When the full depletion of the sensor is reached all the extra current is collected by the guard ring. (Right) Current collected by the same terminals before the onset of the extra current observed beyond 25 V. The effect of the depletion of the gain layer under the pixels and power lines is visible above 5 V.

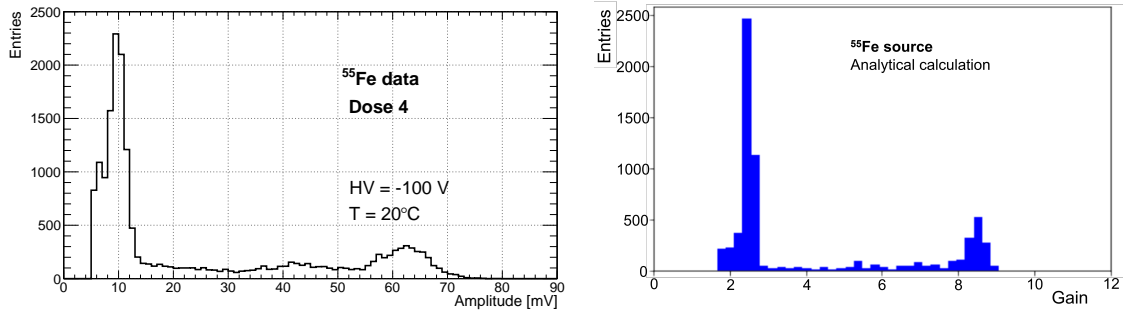
## 6 Measurements with a $^{55}\text{Fe}$ radioactive source

The response in gain of the proof-of-concept PicoAD prototype sensors was studied using a  $^{55}\text{Fe}$  source. The measurements were performed in a climate chamber at an ambient temperature between  $-20$  and  $+20^\circ\text{C}$ . The output of the analog pixels were sent to an oscilloscope with 1 GHz analog bandwidth and the waveforms were acquired for offline analysis.

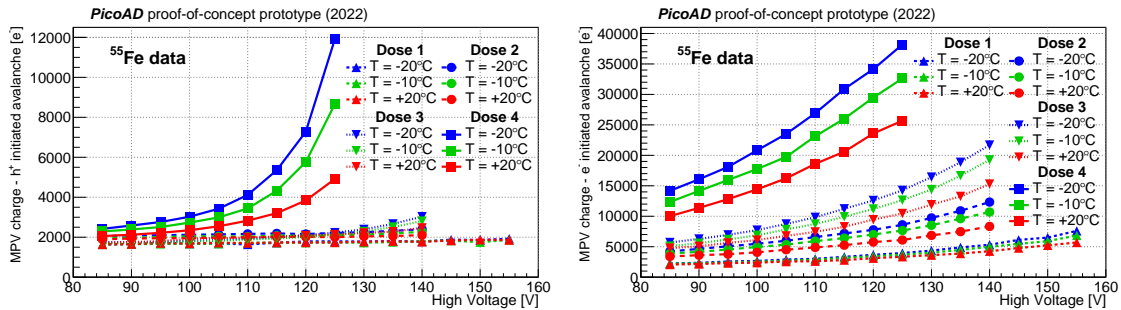
The 5.9 keV photons emitted by the  $^{55}\text{Fe}$  X-ray source interact via photoelectric effect in the silicon, producing a charge cluster inside the sensor that can be approximated as a point-like charge deposition of 1640 electrons. Figure 10 left shows an example of the signal amplitude distributions obtained with the  $^{55}\text{Fe}$  source from a dose 4 sample. The peak in amplitude visible at 10 mV can be attributed to X-ray photons that convert inside the PicoAD drift region; in this case, holes will drift towards the gain region and produce *hole gain*. Conversely, the peak at 63 mV can be attributed to photon conversions within the thin absorption region; in this case, the primary electrons will drift towards the gain layer, producing the much larger *electron gain*. The flat region of the spectrum between the two peaks can be associated to photons that convert either in the inter-pixel area, where the gain is lower, or inside the gain layer. For a qualitative comparison, the same spectrum was produced using the electric field profile extracted from TCAD simulations and calculating the gain with the impact multiplication formula of [16] for primary clusters uniformly distributed in the sensor volume. The result, shown in figure 10 right, supports the interpretation given above.

The gain calculation shown in figure 6 obtained with TCAD transient simulation also corroborates this interpretation.

The mean amplitudes associated to the two peaks were extracted with Gaussian fits. The values were normalized by the gain of the charge amplifier to obtain the collected charge. Figure 11 shows the average collected charge for the hole-gain (left) and electron-gain (right) peaks of the  $^{55}\text{Fe}$  spectrum as a function of the HV for the four gain-layer implant doses, measured at temperatures between  $-20$  and  $+20^\circ\text{C}$ . All sensors show an increase of the signal mean collected charge with increasing sensor bias, which indicates that electron (hole) gain is present for charge clusters produced in the absorption (drift) region.



**Figure 10.** (Left) Signal amplitude spectrum measured with a  $^{55}\text{Fe}$  source for a dose 4 PicoAD sample at a temperature of  $+20^\circ\text{C}$  and high voltage of 100 V. (Right) Gain spectrum obtained using the electric field profiles from TCAD simulation and the analytical formula given in [16] for the gain obtained from impact ionization.

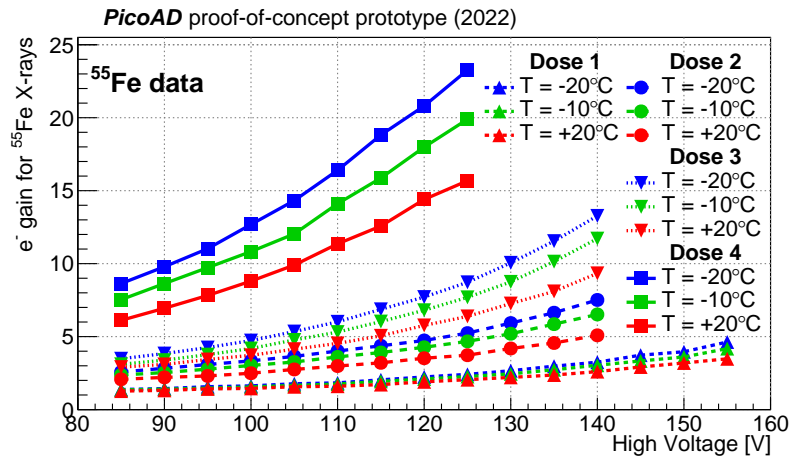


**Figure 11.** Average collected charge of the signals produced in the PicoAD by the conversion of X-ray photons from a  $^{55}\text{Fe}$  source. (Left) with hole gain produced by photon conversion in the drift region. (Right) with electron gain produced by photon conversions in the absorption region.

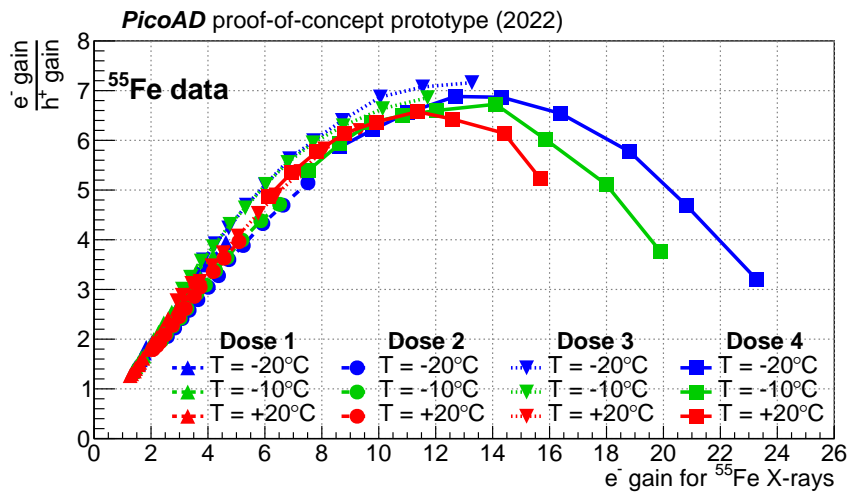
To extract the sensor gain, it was assumed that for each measured temperature the average charge of the first (hole) peak at the lowest measured bias voltage of 85 V and for the lowest gain layer doping concentration (dose 1), corresponds to the signal charge expected in absence of avalanche gain. This value was then used to normalize the average charges of the second (electron) peak at different bias voltages to estimate the gain for avalanches initiated by electrons in the absorption region. Figure 12 shows the result.

A maximum electron gain of 23 was observed for the sensor with gain-layer implant dose 4, operated at the lowest ambient temperature of  $-20^\circ\text{C}$ . Coherently with the expectation, sensors with lower gain-layer implant dose show lower electron gain at a fixed bias voltage.

The PicoAD structure offers the opportunity to study the relation between the electron and hole gain in the same junction, which can be used to infer the properties of the avalanche. Figure 13 shows the ratio between electron gain and hole gain as a function of the electron gain. The hole gain was computed with the same method used for the electron gain and described above. This representation of the data removes the direct dependence of the gain on the temperature and the sensor bias, showing only the characteristics of the impact multiplication in silicon, that in turn depends on parameters of the gain layer, such as its width or the magnitude of the electric field.



**Figure 12.** Gain measured for the conversion of X-ray photons from a  $^{55}\text{Fe}$  source for electron-initiated avalanche as a function of the sensor bias voltage. For each temperature, the gain is obtained as the ratio between the mean collected charge of signals generated by 5.9 keV photon conversion in the PicoAD absorption layer and the mean value obtained at 85 V for conversions in the drift region in the sensor with gain-layer dose 1.

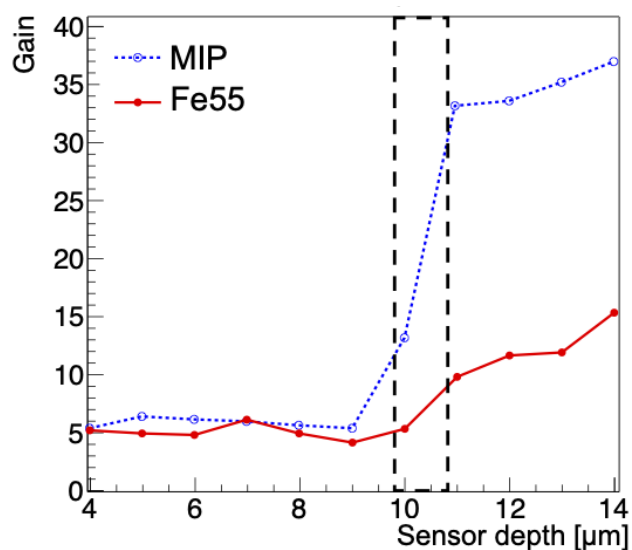


**Figure 13.** Ratio between the electron gain and the hole gain obtained with a  $^{55}\text{Fe}$  source for the four devices tested, as a function of the electron gain.

As expected, all the devices are on the same trend curve, since the implantation energy used for the different doses are the same. For the sensor with dose 4, which shows the highest absolute electron gain, a reduction of the electron/hole gain ratio is measured for electron gains larger than 12. This observation cannot be reproduced by the model of the impact ionization with any parametrization for the impact parameters [16].

The reduction of the gain ratio at large values of electron gain can be explained by transient space-charge effects during the development of the avalanche, which would reduce the electric field in the gain layer at high gain when the primary cluster is produced in the absorption region. The time-dependent spatial charge density varies with the total charge drifting inside the sensor, which is

the product of the gain and the primary charge. The same TCAD simulation introduced in section 4 to obtain the gain profile inside the sensor can be used to estimate the impact of space-charge effects on the measured electron gain. Figure 14 compares the gain profile expected for a primary charge deposited at



**Figure 14.** TCAD simulation of the gain of a point-like primary charge deposition at the center of a PicoAD pixel and at varying depth of 63 electrons (MIP, blue dotted curve, also shown in figure 6) and 1640 electrons ( $^{55}\text{Fe}$  X-ray conversion, red curve). The black dashed lines indicate the high field region produced by the gain layer.

different sensor depths at the center of the pixel. Primary charges of 63 and 1640 electrons were used, the first representing the ionisation of a MIP in 1  $\mu\text{m}$  and the latter the charge deposited by photoelectric effect by an X-ray from the  $^{55}\text{Fe}$  source. The simulation confirms that the large electric-charge density present in the case of  $^{55}\text{Fe}$  X-ray photon conversion limits considerably the gain for an avalanche initiated by electrons, while it has little to no impact when the avalanche is initiated by holes. This result might explain the behavior observed at high electron gain in figure 13. It also suggests that the actual electron gain achievable with MIPs is much larger than the value measured with the  $^{55}\text{Fe}$  source.

## 7 Conclusions

Proof-of-concept prototypes of the monolithic PicoAD were produced at IHP using 5  $\mu\text{m}$  (absorption) + 10  $\mu\text{m}$  (drift) thick epitaxial layers. The prototypes are functional. Probe station transient IV measurements show a depletion of the gain layer compatible with expectations.

Measurements with a  $^{55}\text{Fe}$  X-ray source show a dependence of the electron gain on the dose of the gain layer compatible with the expectations. The highest electron gain measured with  $^{55}\text{Fe}$  source is 23. The PicoAD structure allows measuring electron and hole gain on the same device. The ratio between the electron gain and hole gain deviates from the trend predicted by the model for the charge multiplication produced by impact ionization. This deviation is compatible with a reduction of the electric field during the development of the electron-initiated avalanche for a high-density primary charge deposition. A TCAD transient simulation comparing the gain for a point-like charge deposition from a  $^{55}\text{Fe}$  X-ray source to the one expected for the charge density of a MIP corroborates this hypothesis.

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